

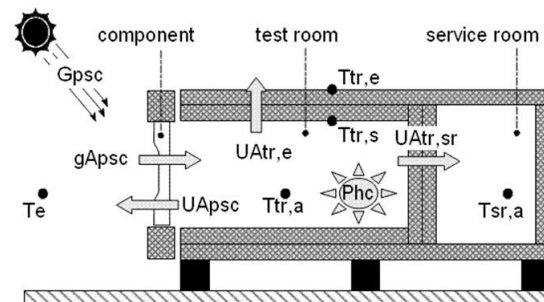
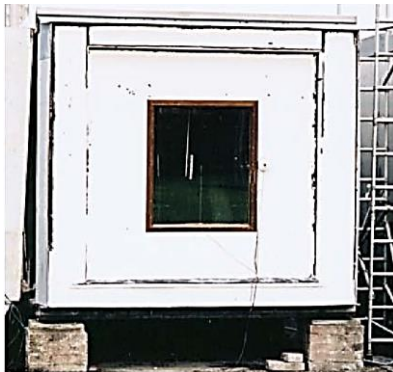
Introduction to LORD

Dr Paul Baker



Origins

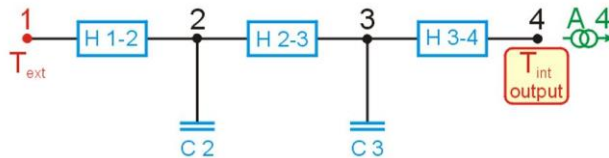
- LORD was developed for the PASLINK EEIG by Olaf Gutschker, BTU Cottbus, to analyse **dynamic test cell data** and deliver high quality performance characteristics for building components tested in real climates.



Purpose

- LORD can be used for components (walls, windows etc), whole rooms or more complicated systems;
- to obtain **thermal transmittance values, solar gain factors**, and possibly dynamic information (e.g. capacitances, time constants).
- A transient mathematical model is assumed. The parameters of the model (e.g. resistances, capacitances and heat flow admittances) essentially define the dynamic and steady-state thermal and solar properties of the system.

RC-networks



- Initial guesses of the parameter values are made.
- The **output** of the actual test (for instance, the test room temperature T_{int} as a function of time) is compared with the **output** which the model produces for the same **input** conditions.
- By statistical analysis of the deviations between the model and the measured outputs, the parameter values are progressively adjusted in order to improve the agreement.
- Read LORD Manual and other documents which will be provided.

(Mostly) User friendly interface

Step 1 - Input data



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File formats – tab delimited or CSV

Headers must be enclosed in single quotation marks

	A	B	C	D	E	F	G
1	'timestamp'	'Tsi_glazing'	'Tsi_left'	'Tsi_back'	'Tsi_right'	'Tsi_ceiling'	'Tsi_floor'
2	41614	22.7454834	26.606781	26.6628572	27.2989349	26.4609832	28.63676
3	41614.00694	22.5884704	26.4465637	26.4946289	27.1242904	26.2911529	28.49256
4	41614.01389	22.4506836	26.2751311	26.3376159	26.9624634	26.134137	28.34516
5	41614.02083	22.3161011	26.1245224	26.1822051	26.7862244	25.9658966	28.19936
6	41614.02778	22.1959381	25.9626922	26.0299851	26.6083832	25.7912597	28.04554
7	41614.03472	22.0549438	25.7896576	25.8681641	26.4337463	25.6230316	27.91416
8	41614.04167	21.9043121	25.6278382	25.7063447	26.263916	25.4532013	27.77157

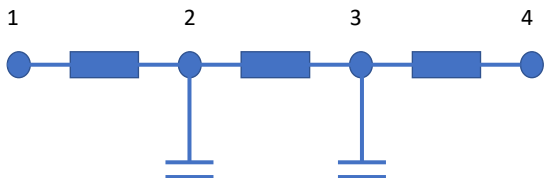
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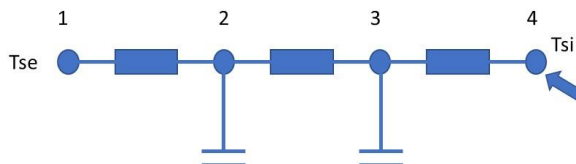
Step 2 – Create a model

Usually set capacitances at internal and external nodes to zero.

Check that time step is correct (note default is 60 minutes)

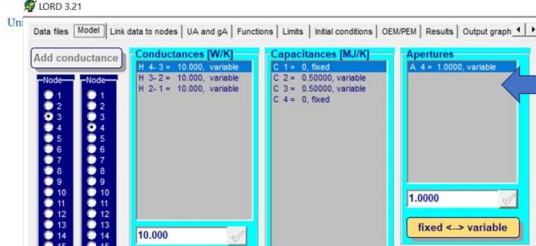


Step 3 – Link data to nodes

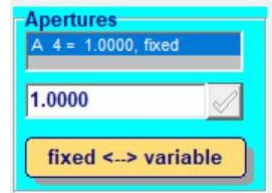


We now have a basic four node model which could be applied to heat flow measurements through a wall.

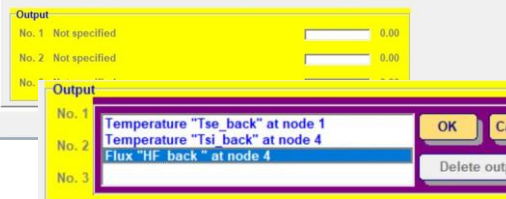
Step 4 – Go back to Model!



Fix Aperture = 1
for measured *Heat Flux* or *Heating Power*



Select Output



For *Solar Radiation Aperture* is **variable**.



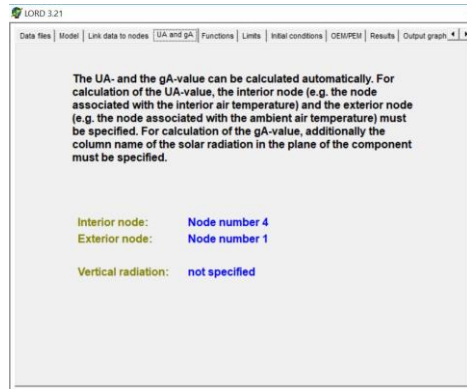
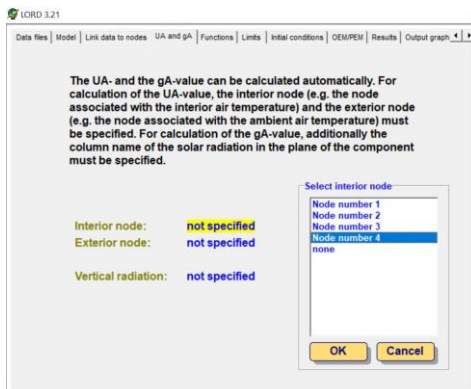
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Step 5 - UA & gA

Note for 1-D heat flux measurements = U- & g-values

For our 4-node model we need to specify interior & exterior nodes:



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Step 6 – Initial Conditions

LORD 3.21

Data files | Model | Link data to nodes | UA and gA | Functions | Limits | Initial conditions | OEM/PEM | Results | Outp

The temperatures at the nodes 2 and 3 will be calculated during the run of the program. For the first timestep (initial conditions) the temperatures of these nodes shall be ...

Identified like variable parameters

let constant at T = 20 °C

let constant at their actual values

Step 7 – Limits

LORD 3.21

Data files | Model | Link data to nodes | UA and gA | Functions | Limits | Initial conditions | OEM/PEM | Results | Output graph

<input checked="" type="checkbox"/>	H 03-02	: 1.000E-0001 ... 2.000E+0003
<input type="checkbox"/>	H 01-02	: 1.000E-0001 ... 2.000E+0003
<input checked="" type="checkbox"/>	H 04-03	: 1.000E-0001 ... 2.000E+0003
<input checked="" type="checkbox"/>	C 02	: 1.000E-0005 ... 5.000E-0001
<input checked="" type="checkbox"/>	C 03	: 1.000E-0005 ... 5.000E-0001
<input checked="" type="checkbox"/>	T 02	: -2.000E+0001 ... 8.000E+0001
<input checked="" type="checkbox"/>	T 03	: -2.000E+0001 ... 8.000E+0001

Check boxes to activate the limits

Parameter H 04-03

Lower limit: 1.000E-0001

Upper limit: 2.000E+0003

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Step 8 – OEM/PEM

LORD 3.21

Data files | Model | Link data to nodes | UA and gA | Functions | Limits | Initial conditions | OEM/PEM | Results | Output graph

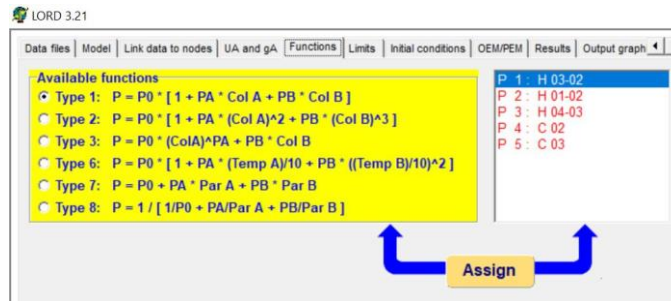
Output Error Method Prediction Error Method

- In general, the residuals using PEM are smaller than using OEM.
- The identification process takes much longer using PEM.
- PEM can only be used if the outputs are measured temperatures.
- Ask a statistician to explain!

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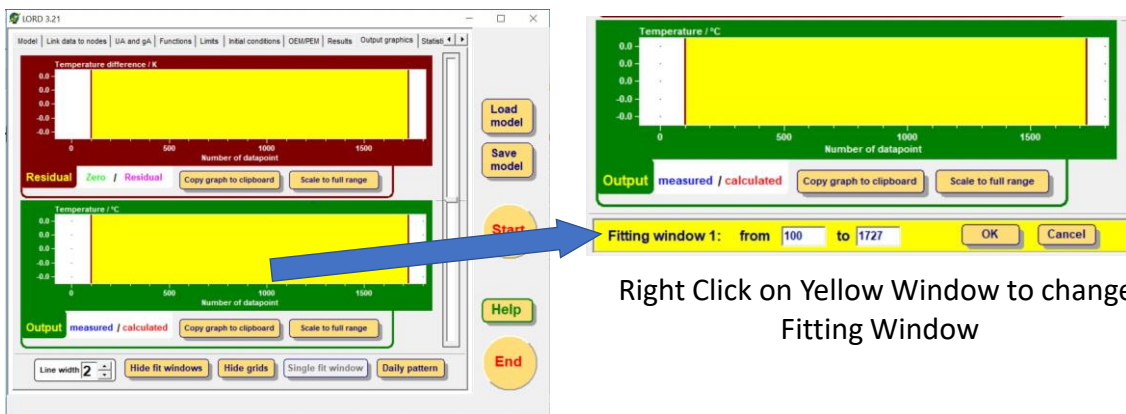
Other Options - Functions



For example, it is possible to create a variable resistance dependent on a measured parameter such as wind speed.

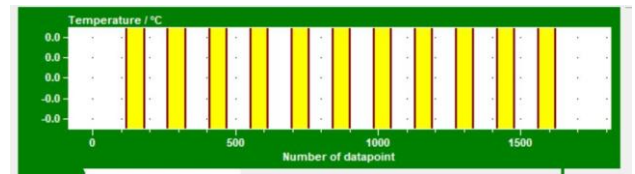
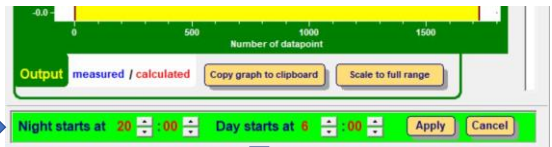
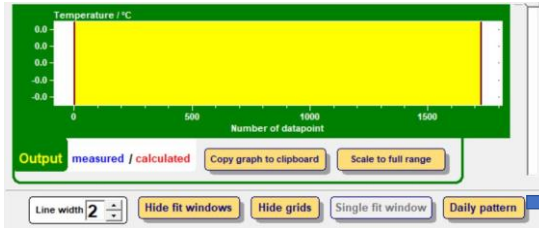
Options – Output Graphics & ‘Fitting Windows’

- Fitting windows can be used to select only part of the data for analysis.
- See LORD help for instructions.



Right Click on Yellow Window to change Fitting Window

Daily Pattern



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Run!



LORD 3.21

Model | Link data to nodes | UA and gA | Functions | Limits | Initial conditions | OEM/PEM | Results | Output graphics | Statistics

Notation in scientific format	
Par. 1 : H 03-02 = 2.735 W/K	± 3.4 %
Par. 2 : H 01-02 = 0.616 W/K	± 0.8 %
Par. 3 : H 04-03 = 38.822 W/K	± 4.8 %
Par. 4 : C 02 = 0.116 MJ/K	± 2.8 %
Par. 5 : C 03 = 0.222 MJ/K	± 1.0 %
Par. 6 : T 02 = -19.991 °C	± > 100 %
Par. 7 : T 03 = -19.951 °C	± > 100 %

Downhill Simplex Method

Monte-Carlo Method

Actual Residual :
0.64307688 W

Number of Iterations:

Downhill Simplex:	14806
Monte-Carlo:	883480
Total number:	898286
Last improvement at step:	753106

UA = 0.496 W/K ± 0.2 %

gA = not calculable
(see "UA and gA" page)

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Results - Output File *.log gives all input and output information

```

Back10min-5 - Notepad
File Edit Format View Help
Log-File, created by LORD
*****
Date: 17/08/2020
Time: 14:39:33
Time step: 10.00 minutes
Fitting window:
number 1 - from 100 to 4751
*****
Model and start values
*****
Conductances [W/K]
-----
H 4- 3 = 38.822, variable, limited between 0.10 and 2000.00
H 3- 2 = 2.7952, variable, limited between 0.10 and 2000.00
H 2- 1 = 0.05010, variable
-----
Capacitances [MJ/K]
-----
C 1 = 0, fixed
C 2 = 0.11647, variable, limited between 0.000 and 0.500
C 3 = 0.22200, variable, limited between 0.000 and 0.500
C 4 = 0, fixed
-----
Apertures
-----
A 4 = 1.0000, fixed
-----
Parameter Functions
-----
not specified
-----
Columns in the data file and links to nodes
-----
Node number 1 ----> temperature "Tse_back"
Node number 4 ----> temperature "Tsl_back"
Node number 4 ----> flux "hf_back"
-----
Outputs
-----
No.1: File "hf_back" at node 4, weight = 1.00
No.2: Not specified
No.3: Not specified
-----
Initial conditions
-----
Initial temperatures were identified.
  
```

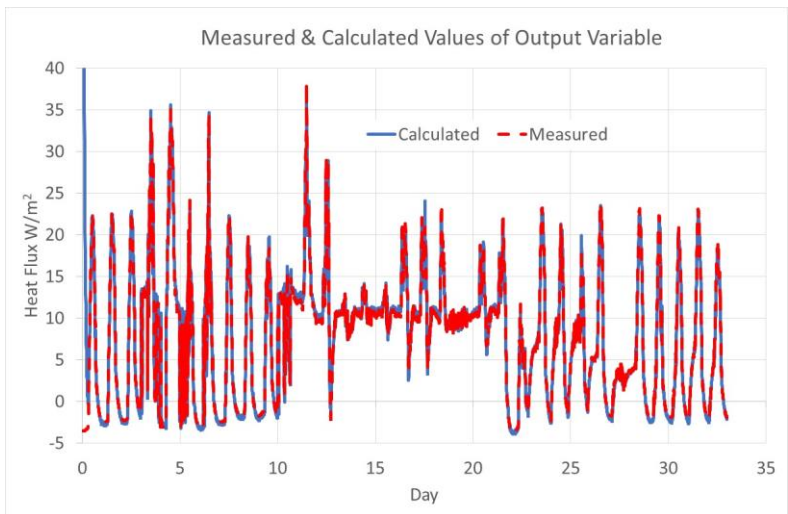
```

=====
Results
=====
-----
Iterations
-----
Downhill Simplex Method: 31800
Monte Carlo Method: 972710
Total number of iterations: 1004510
Last improvement at step: 943995
-----
Residual at end of calculation: 0.64307645 W
-----
Parameters
-----
Par. 1 : H 03-02 = 2.722 W/K ± 3.4 %
Par. 2 : H 01-02 = 0.657 W/K ± 0.8 %
Par. 3 : H 04-03 = 20.702 W/K ± 4.0 %
Par. 4 : C 02 = 0.0124 MJ/K ± 2.8 %
Par. 5 : C 03 = 0.0370 MJ/K ± 1.0 %
Par. 6 : T 02 = -19.096 °C ± 100 %
Par. 7 : T 03 = -19.052 °C ± 100 %
-----
UA and gA
-----
Interior node: Node number 4
Exterior node: Node number 1
Column with vertical radiation: not specified
-----
UA and gA
-----
Interior node: Node number 4
Exterior node: Node number 1
Column with vertical radiation: not specified
-----
UA = 0.406 W/K ± 0.1 %
gA = not calculable
-----
Cross - Correlation
-----
-----
| H 03-02 | H 01-02 | H 04-03 | C 02 | C 03
-----
H 03-02 | 1.0000 | -0.5792 | 0.0133 | 0.0285 | -0.3529
H 01-02 | -0.6792 | 1.0000 | -0.0000 | -0.0000 | 0.3028
H 04-03 | 0.0133 | -0.0000 | 1.0000 | 0.2362 | -0.2584
C 02 | 0.0285 | -0.0000 | 0.2362 | 1.0000 | -0.4843
C 03 | -0.3529 | 0.3028 | -0.2584 | -0.4843 | 1.0000
  
```

Results - Output File *.res gives measured & calculated values of output variable

```

Back_10min-5 - Notepad
File Edit Format View Help
Day      Calc. 1 Meas. 1
0.0069444 1122.4832 -3.5312
0.0138889 710.7753 -3.5433
0.0208333 461.6966 -3.5464
0.0277778 309.8872 -3.5555
0.0347222 216.0325 -3.5646
0.0416667 157.2057 -3.5706
0.0486111 119.2652 -3.5676
0.0555556 94.4965 -3.5433
0.0625000 77.8772 -3.5585
0.0694444 65.5455 -3.5706
0.0763889 56.3539 -3.5494
0.0833333 49.1957 -3.5585
0.0902778 43.4346 -3.5555
0.0972222 38.9503 -3.5525
0.1041667 34.7030 -3.5494
0.1111111 31.0022 -3.5433
0.1180556 27.7674 -3.5191
0.1250000 24.9462 -3.5100
0.1319444 22.8053 -3.5009
0.1388889 20.2331 -3.4888
0.1458333 17.9165 -3.4888
0.1527778 16.0493 -3.4676
0.1597222 14.3594 -3.4646
0.1666667 12.9064 -3.4465
  
```



Save Model

A final option is to run an Error Propagation:

LORD 3.21

UA and gA | Functions | Limits | Initial conditions | OEM/PEM | Results | Output graphics | Statistics | Error propagation

Name of input	Uncertainty	unit	consider ?	UA +	UA -	gA +	gA -	d UA	d gA
EXTERNAL	0.500	K	yes	2.406	2.126	---	---	0.140	---
INTERNAL	0.500	K	yes	2.126	2.406	---	---	0.140	---
HF_Glazing	5.000	%	yes	2.371	2.145	---	---	0.113	---

Actual Residual :
0.902 W

Load model

Save model

Start

Help

End

Results with undisturbed inputs:
UA = 2.258 W/K
gA = not calculable

Total error (root mean square):
d UA = 0.228 W/K (10.1 %)
d gA = not calculable


Start Error propagation

Stop Error propagation

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Using LORD for Simulation/Validation

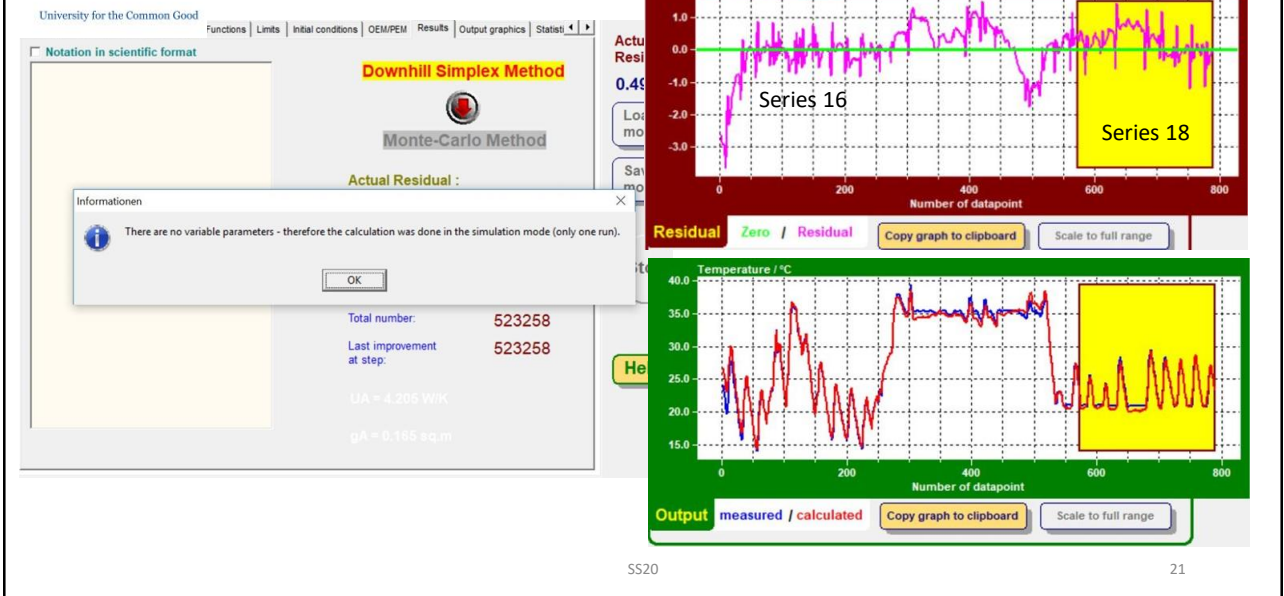
- Example: validate results from one part of a data series on another part – identify model on Series 16 and apply to Series 18.
- Run LORD for Series 16 only.
- Obtain results & save model.
- Fix all parameters.
- Set initial conditions. 
- Move window over Series 18.
- Run LORD.

- identified like variable parameters
- let constant at T = 20 °C
- let constant at their actual values

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Using LORD for Simulation/Validation

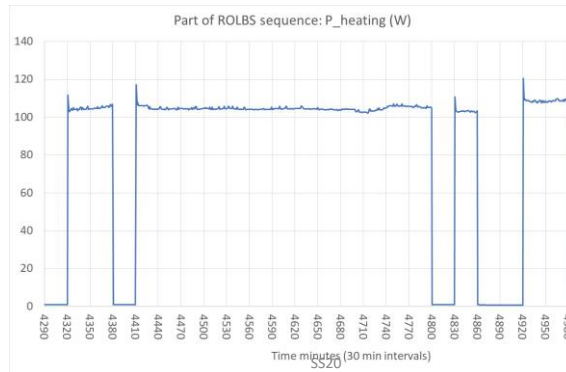


Application of LORD to Real Data

- Firstly the data must be processed for input in LORD
 - Check integrity of data – plots!
 - Missing data?
 - Anomalies?
 - What data interval to use? *Example of PSA Series 16-18 data follows.*
 - Etc.

What is the optimum data interval in order *not* to lose dynamic information?

- Data are provided at 1 minute intervals (too much information – too long computation time?)
- The ROLBS sequence in Series 16 is based on 30 minute periods:



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- Maximum interval to include all dynamic information is 30 minutes,
- Maybe better to use 10 minute averages.
- Check data to identify start of ROLBS:

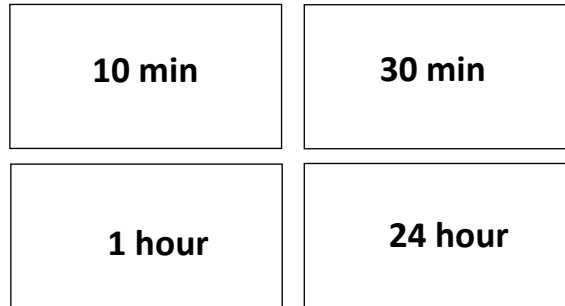
A	B	C	E	F	G	H	J	K	L	M	N	O	P	Q	R	S	T	V	X	AA	AY	AZ
																						P_heating
09/12/2013 01:21	4402																					
09/12/2013 01:22	4403																					
09/12/2013 01:23	4404																					
09/12/2013 01:24	4405																					
09/12/2013 01:25	4406																					
09/12/2013 01:26	4407																					
09/12/2013 01:27	4408																					
09/12/2013 01:28	4409																					
09/12/2013 01:29	4410																					
09/12/2013 01:30	4411																			117.2594	09/12/2013 01:30	105.7771495
09/12/2013 01:31	4412																					
09/12/2013 01:32	4413																					
09/12/2013 01:33	4414																					
09/12/2013 01:34	4415																					
09/12/2013 01:35	4416																					
09/12/2013 01:36	4417																					
09/12/2013 01:37	4418																					
09/12/2013 01:38	4419																					

Inspect data: Sequence changes on the hour or half hour.

Therefore start averaging at the beginning of Series 16 at 6/12/13 00:00

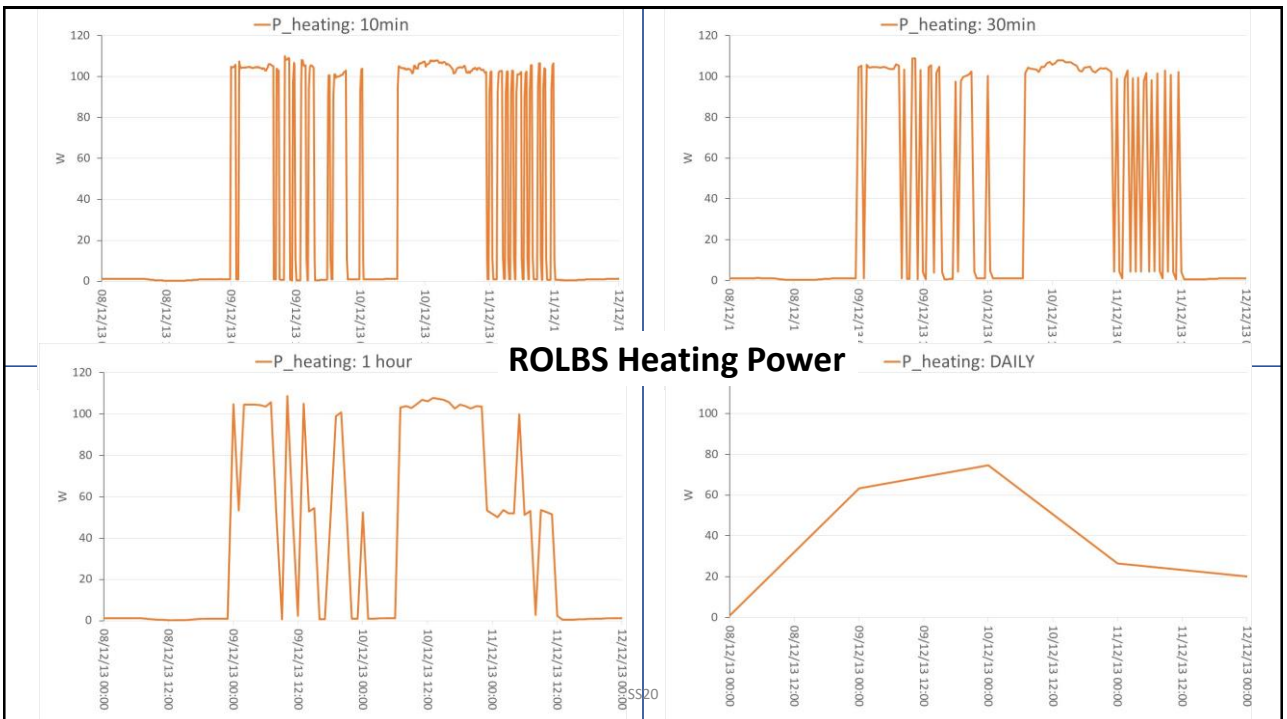
This captures all the dynamic information.

The following figures show the effect of different averaging periods....

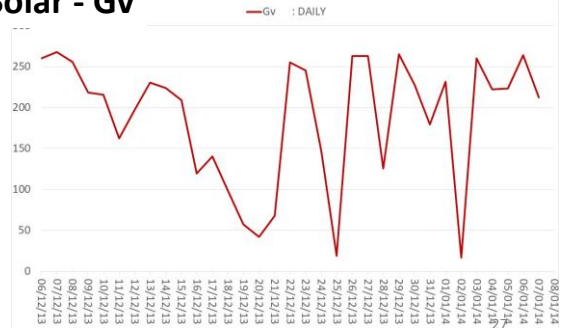
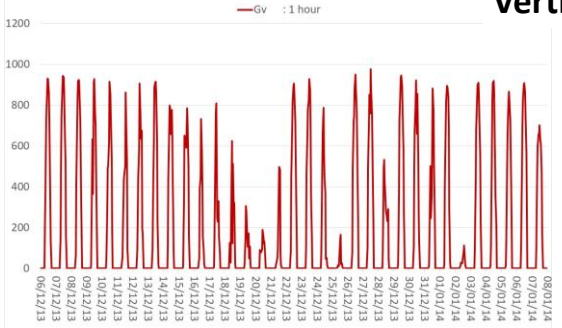
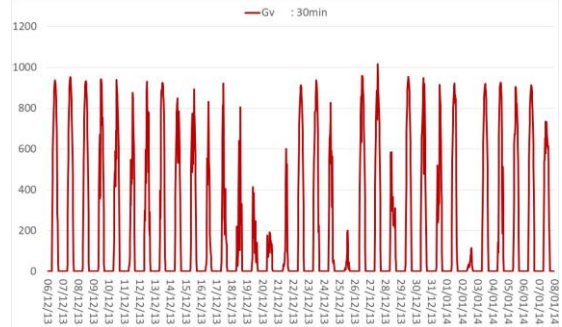
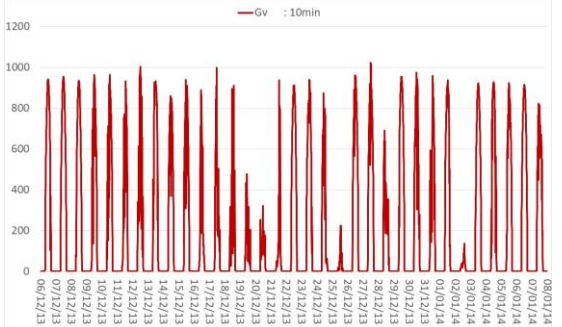


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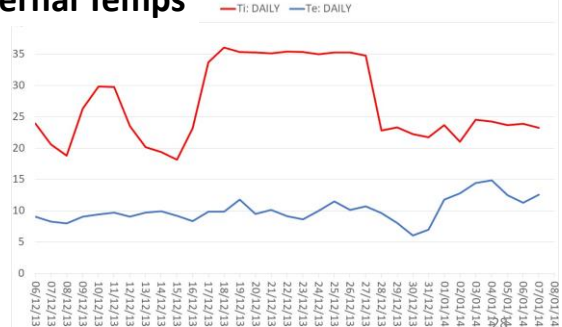
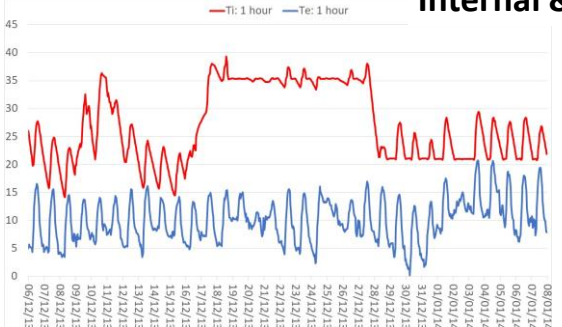
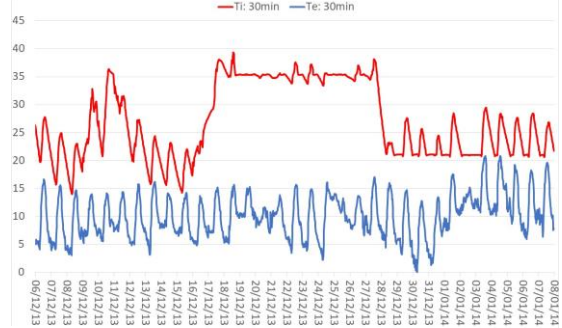
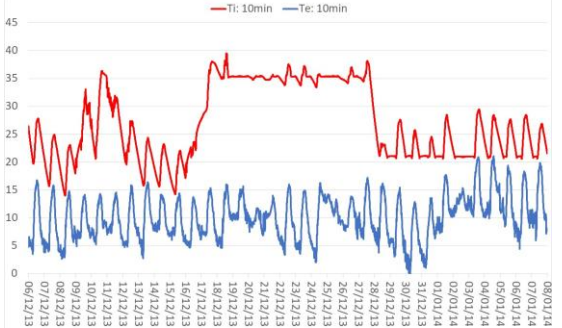


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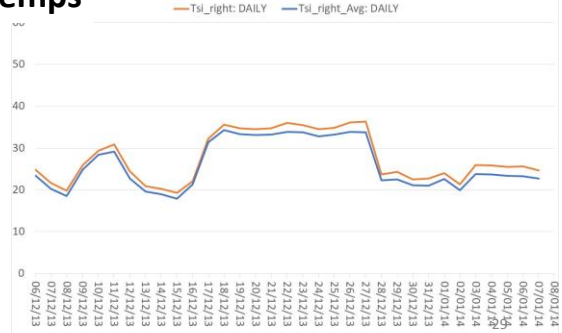
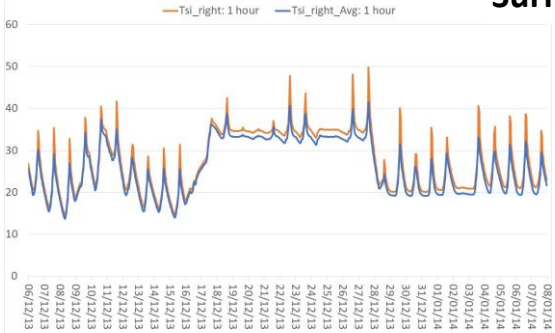
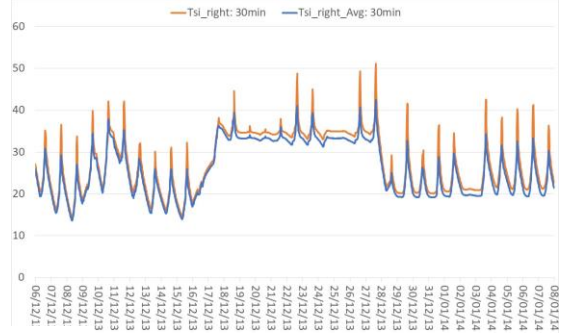
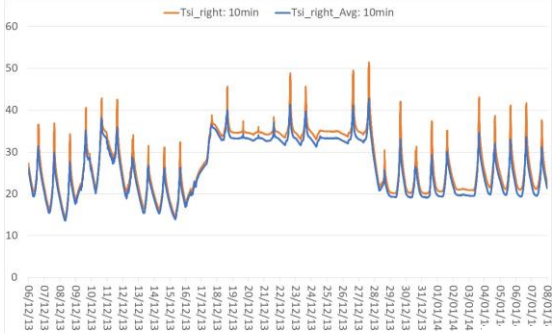
Vertical Solar - Gv

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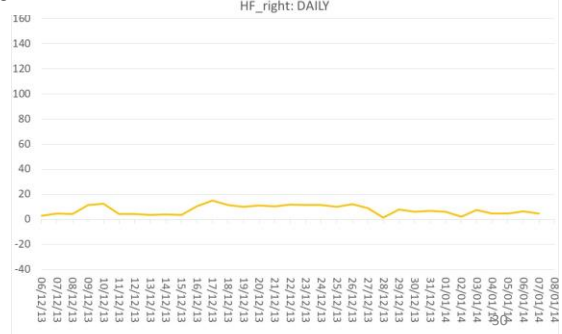
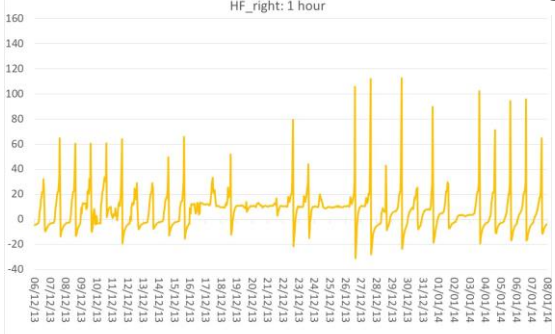
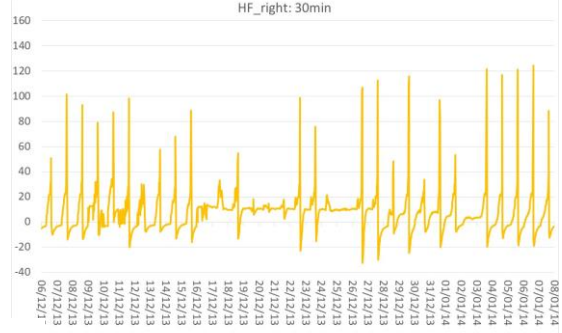
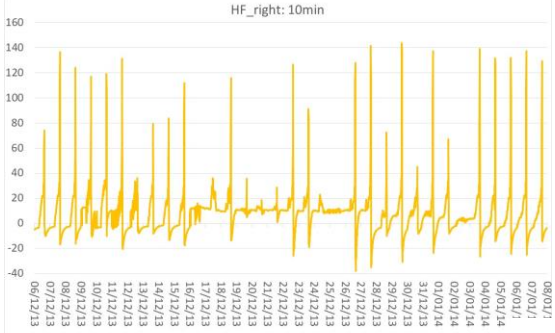
Internal & External Temps

SS20



Surface Temps

SS20



Heat Flux

SS20

Applying LORD to Heat Flux Measurements from PSA data

- Firstly it is helpful to estimate results by *simple averaging* before running LORD on data.
- I've tried three approaches using the different temperatures available.....
- These give a good idea of the U-value result(s) you should be aiming for by identification.

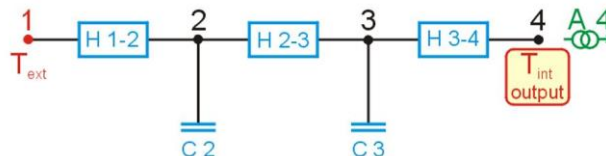
U-value based on Tsi, Tse & HF					
	Left	Back	Right	Ceiling	Floor
ALL Data	0.44	0.46	0.41	0.45	0.53
Series 16	0.47	0.48	0.42	0.48	0.57
Series 17	0.45	0.45	0.42	0.45	0.48
Series 18	0.41	0.43	0.37	0.42	0.55
U-value based on Ti, Te & HF					
	Left	Back	Right	Ceiling	Floor
ALL Data	0.46	0.45	0.44	0.52	0.55
Series 16	0.49	0.49	0.46	0.56	0.61
Series 17	0.45	0.44	0.44	0.49	0.47
Series 18	0.44	0.44	0.43	0.50	0.59
U-value based on Tsi_Avg, Tse & HF					
	Left	Back	Right	Ceiling	Floor
ALL Data	0.47	0.46	0.44	0.48	0.60
Series 16	0.51	0.49	0.46	0.52	0.67
Series 17	0.46	0.45	0.45	0.49	0.52
Series 18	0.45	0.44	0.42	0.45	0.65

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Using LORD

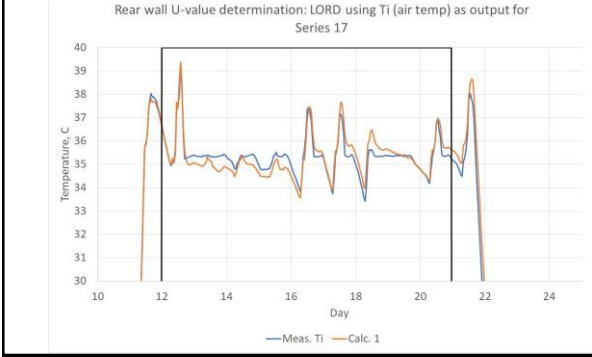
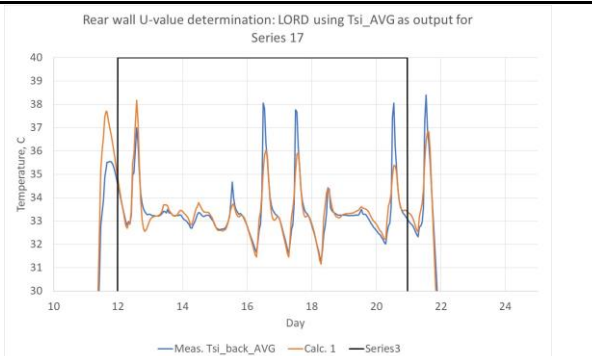
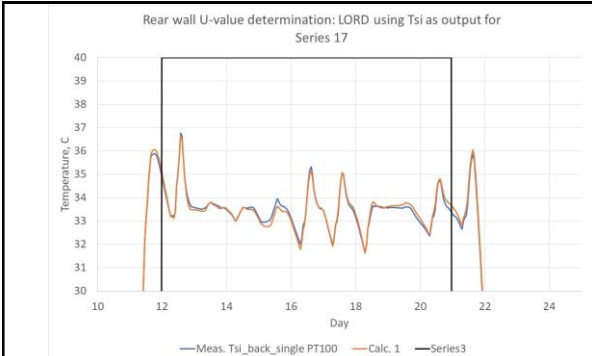
- The rear wall is used as an example.
- Use the basic 4 node model.



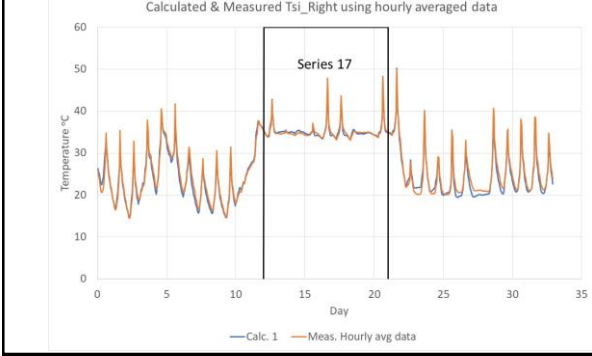
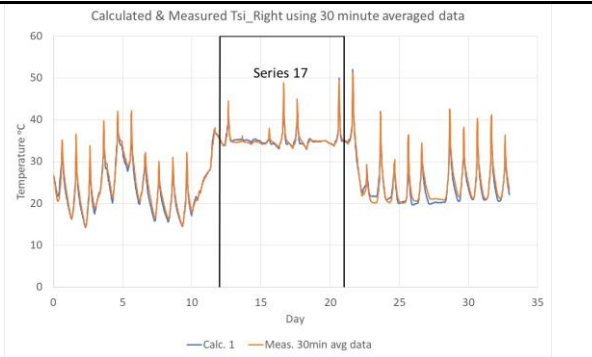
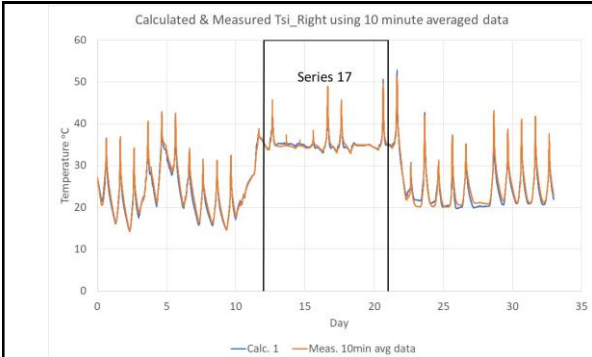
- I've used the external surface temperature Tse and the PT100 internal temperature Tsi because it is more local to heat flux sensor.
- I tried Tsi_Avg and Ti, however Tsi produced better results – lower residuals.

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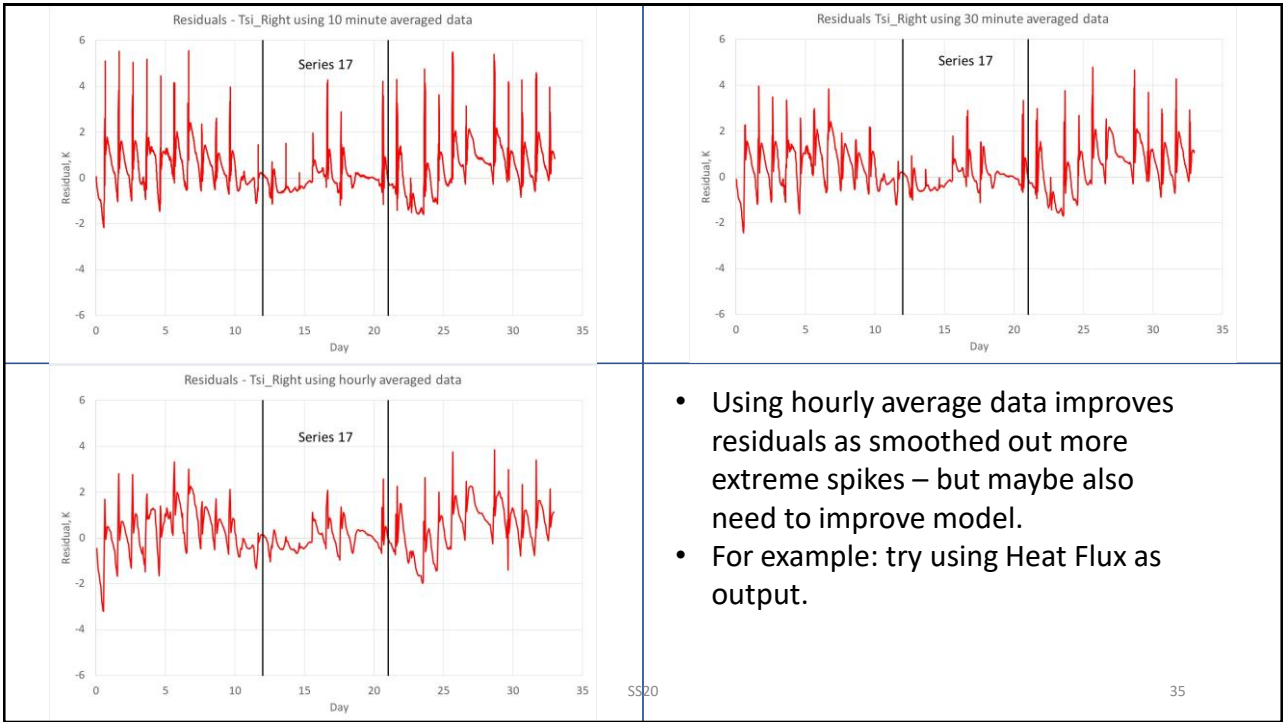
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Tsi appears to give best fit



	Averaging Period	U-value, W/m ² K
LORD	10 min	0.42
LORD	30 min	0.42
LORD	Hourly	0.42
Averaging Method		0.42



UA- & gA-values for whole test cell from Series 16-18 or 'Co-heating' test of a building

- For the heat flux measurements we can easily get an idea of the U-value by the averaging method, however this is not possible for UA- & gA-values.
- For steady state conditions, the electrical heat input to maintain a constant internal temperature within the test cell or building, will increase when the outside temperature falls and decrease when the solar radiation rises (in actuality these are always fluctuating, but dampened by the thermal inertia). However, neither the heat loss coefficient, nor the solar heat gain factor of the building envelope can be measured directly.

- But estimates can be made using the daily average data with **Siviour Analysis** for Series 16-18.....

What is Siviour Analysis?

Daily averages (or longer) are produced.

$$P_{heating} = UA \times \Delta T - gA \times Gv$$

Dividing by ΔT gives

$$\frac{P_{heating}}{\Delta T} = UA - gA \times \frac{Gv}{\Delta T}$$

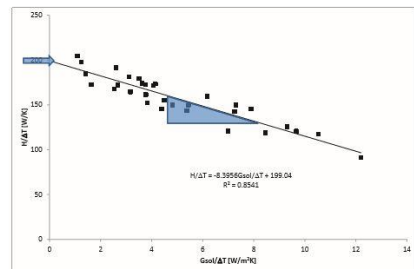
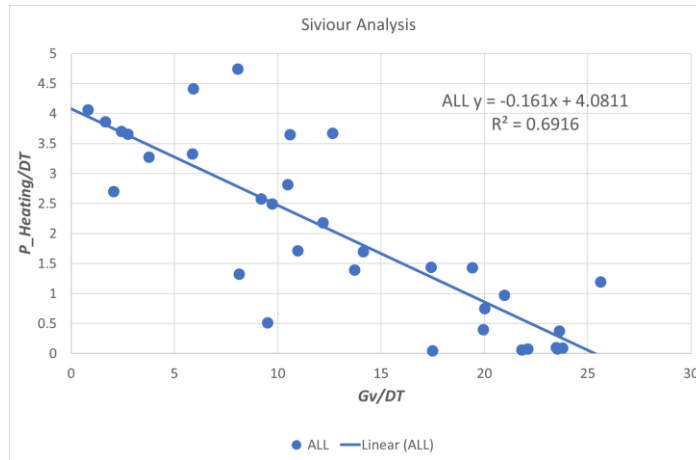


Figure A2: Example of X-Y plot of co-heating test data (Siviour analysis). The intercept of the linear regression line is the whole house heat loss coefficient and the slope is the solar gain factor

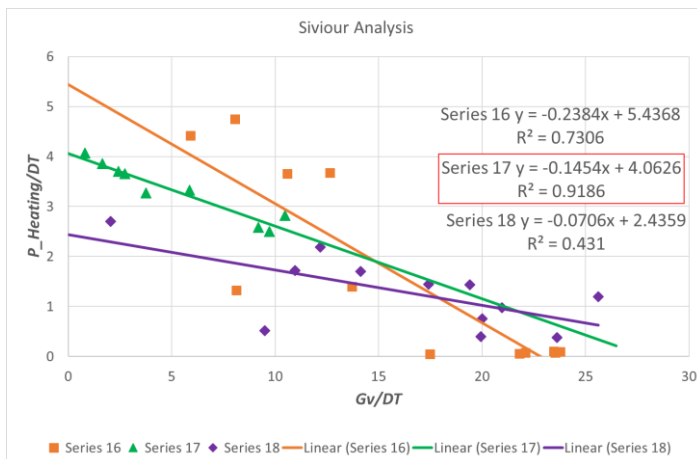
All data Series 16-18



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Divide into 3 series



Series 17 gives the best fit:
UA= 4.06 W/K
gA= 0.145 m²

Best 'steady state' data series with high ΔT

This suggest that the data series would *possibly* give good results for steady state parameters using LORD, etc.

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Research Papers

FIRST EVIDENCE FOR THE RELIABILITY OF BUILDING CO-HEATING TESTS

Richard Jack, Dennis Loveday, David Allinson and Kevin Lomas

*Building Energy Research Group, School of Civil & Building Engineering,
Loughborough University.*

Building Research & Information Vol. 46, 2018.

The energy balance is typically carried out using measurements that are averaged over a 24 hour period:

- Electrical Heating + Solar Heating = Fabric Heat Loss + Infiltration Heat Loss

Co-heating Test Methodologies

In November 2013, NHBC report NF54, Review of Co-heating Test Methodologies, was produced, which contained a background to co-heating testing and an initial analysis of the results (Butler & Dengel, 2013).

It concluded that variable weather conditions, in particular heat gain resulting from **solar irradiance**, were the largest cause of **uncertainty** in the test results.

- *Google also: QUB/e: U-values in-situ*

Multiple Regression Analysis

As an alternative to Siviour Analysis use MRA treating ΔT & Gv as independent variables with the heating power H as the dependent variable.

SUMMARY OUTPUT								
Regression Statistics								
Multiple R	0.9686565							
R Square	0.938295416							
Adjusted R Squar	0.904046881							
Standard Error	13.78066775							
Observations	33							
ANOVA								
	<i>df</i>	<i>SS</i>	<i>MS</i>	<i>F</i>	<i>Significance F</i>			
Regression	2	89520.88797	44760.44399	235.6968952	4.50956E-19			
Residual	31	5887.110913	189.9068036					
Total	33	95407.99889						
	<i>Coefficients</i>	<i>Standard Error</i>	<i>t Stat</i>	<i>P-value</i>	<i>Lower 95%</i>	<i>Upper 95%</i>	<i>Lower 95.0%</i>	<i>Upper 95.0%</i>
Intercept	0	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A
Gv	-0.16674958	0.0210204	-7.932750068	5.90481E-09	-0.209620968	-0.123878191	-0.209620968	-0.123878191
ΔT	4.207991683	0.234685402	17.93035122	6.40728E-18	3.72934765	4.686635716	3.72934765	4.686635716

$gA = 0.17$
 $UA = 4.208$

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Multiple Regression Analysis

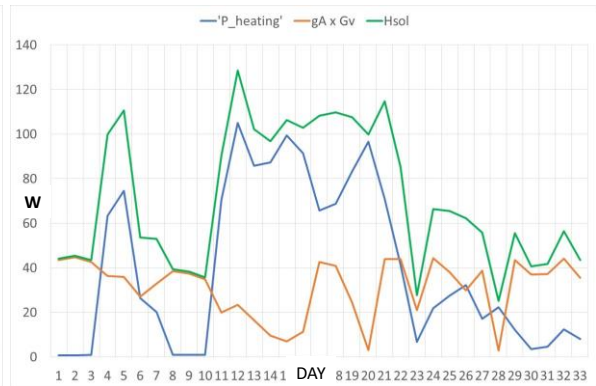
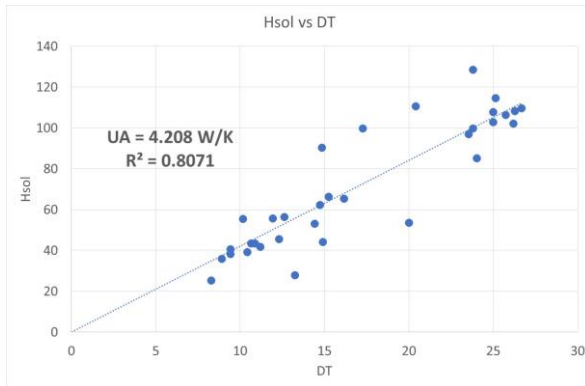
The gA -value result is used to adjust daily values of the heating power for solar gains:

$$H_{sol} = H + gA * Gv = UA \times \Delta T$$

Plot H_{sol} (heating power + solar gains) vs. ΔT

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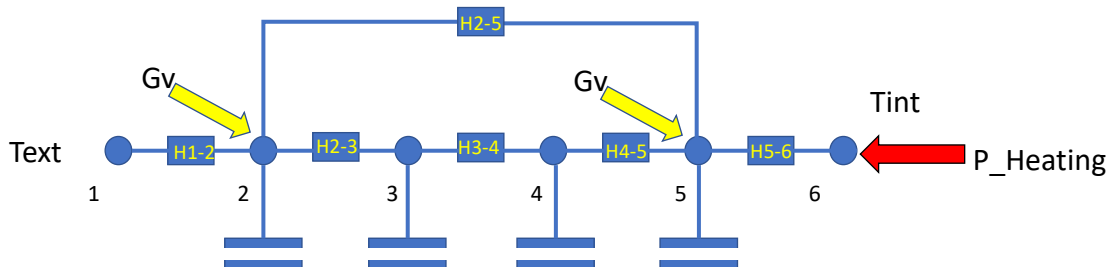


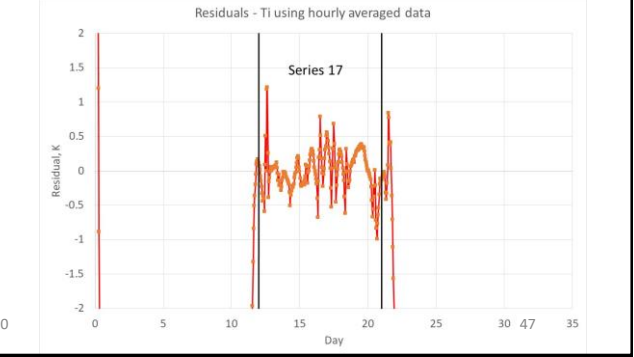
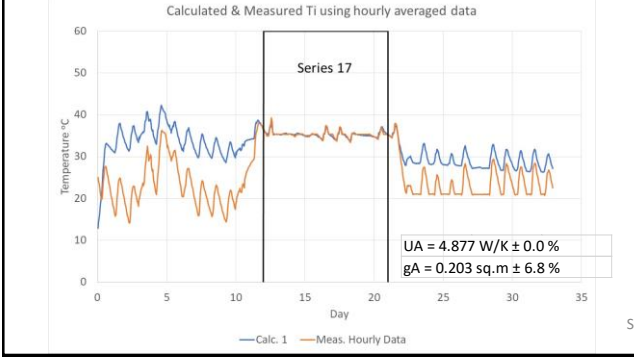
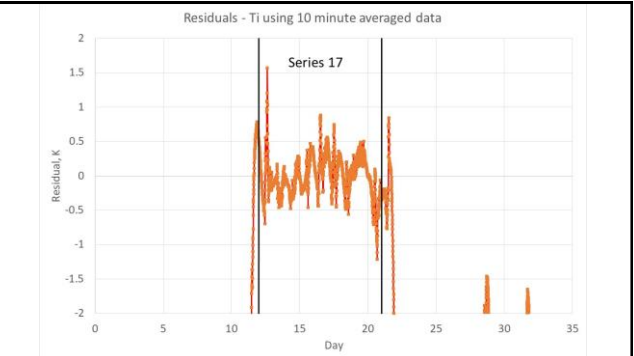
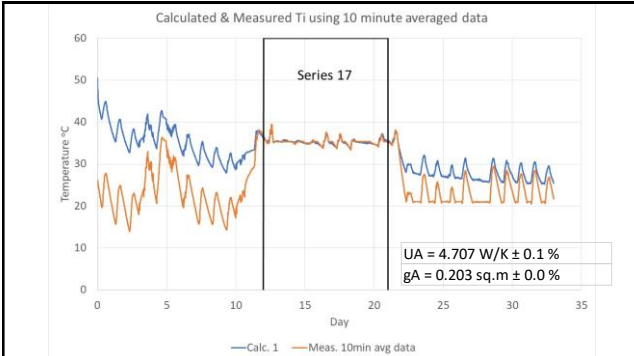
Maybe useful if you're only interested in UA-value.

'Whole Building' model

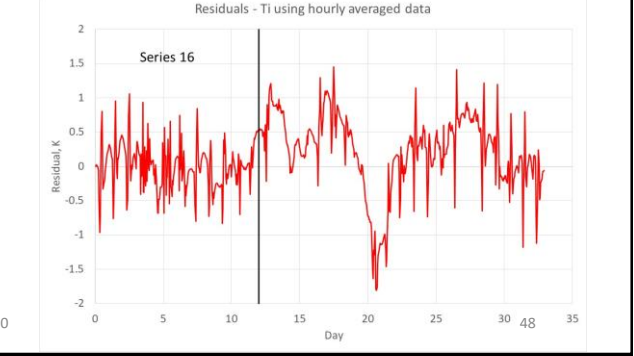
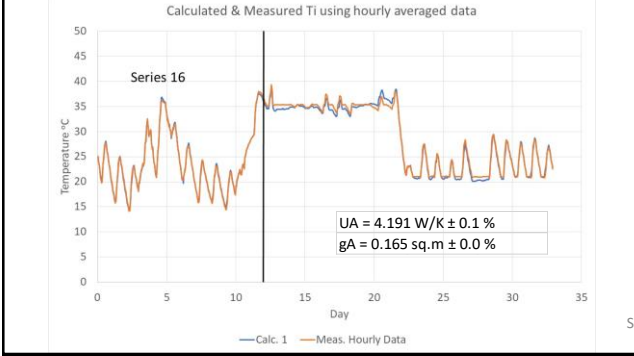
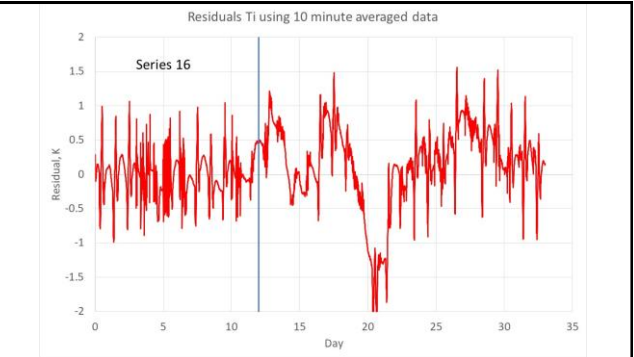
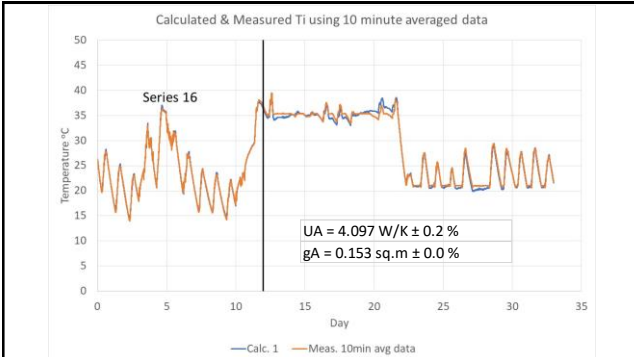
- Represent in LORD with six nodes (could be less!):

The additional parallel conductance H2-5 connected between node 2 and 5 allows for thermal conduction without storage (e.g. a window).





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Results

- Expected the more steady state Series 17 would give good results,
- However UA- & gA-values using Series 17 are high.
- Also the model fit to the rest of the data (Series 16 & 18) is poor.

- Series 16 gives better results and overall a better fit to *all* data.

- Do we use 10min or hourly data?
- Are there problems with high frequency data using LORD?
- Try different model?

Comments & Conclusions

- Important to understand the physical system, for example, the construction of the PSA test cell and sensor locations.
- Plot the data – check for integrity.
- Use simple averaging or Siviour analysis to estimate results prior to using identification techniques.
- Select suitable data averaging period, particularly for dynamic test sequences.
- Compare different parts of test sequences.
- Note: I've not mentioned Capacitance!

Thank You!